



Casing Wear evaluation through simulation

Visegrád, 21 November 2013

Society of Petroleum Engineers



Overview



- Theoretical background
- Candidate well
- Simulation workflow
- Simulation results
- Conclusions



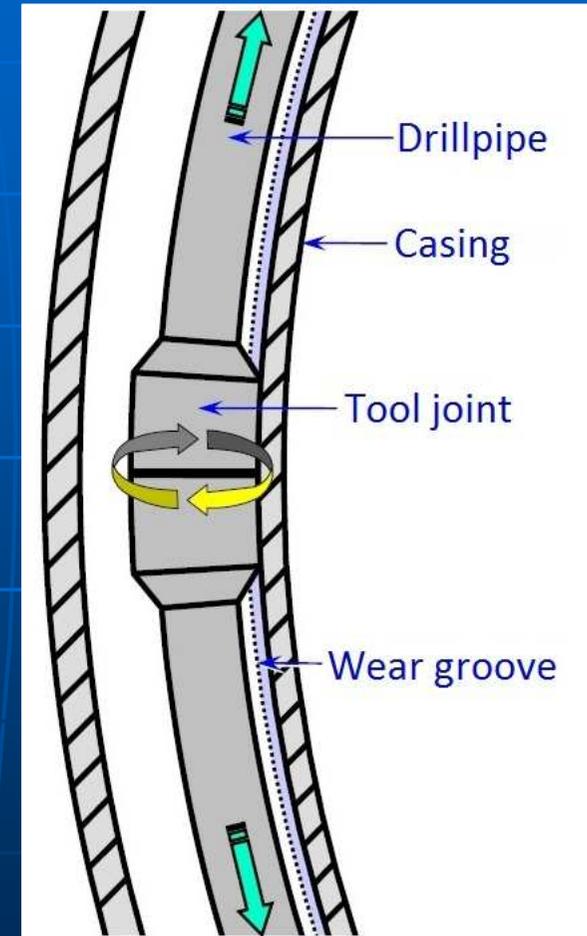
Theoretical background



- Well integrity
 - Reduced burst and collapse pressure
- Well life
 - Future well operations
 - Artificial lift
- Costs
 - Casing remediation
 - Well abandonment

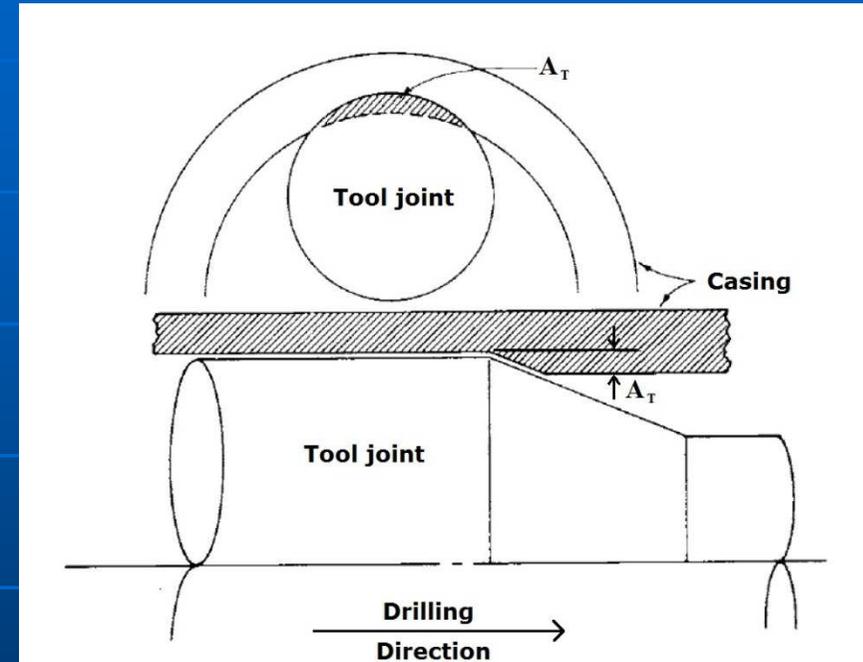
Theoretical background

- Rotating tool joint forced against the casing wall
- Contact causes friction
- Result: Crescent-shaped wear groove



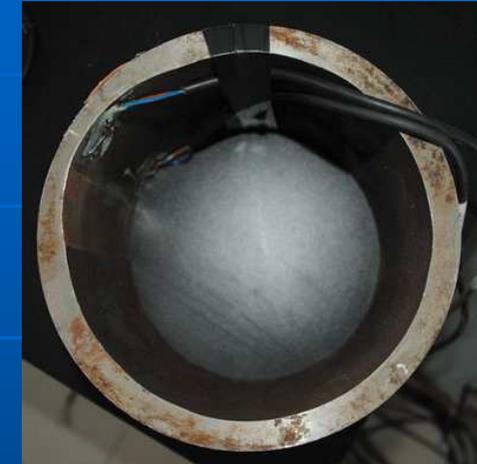
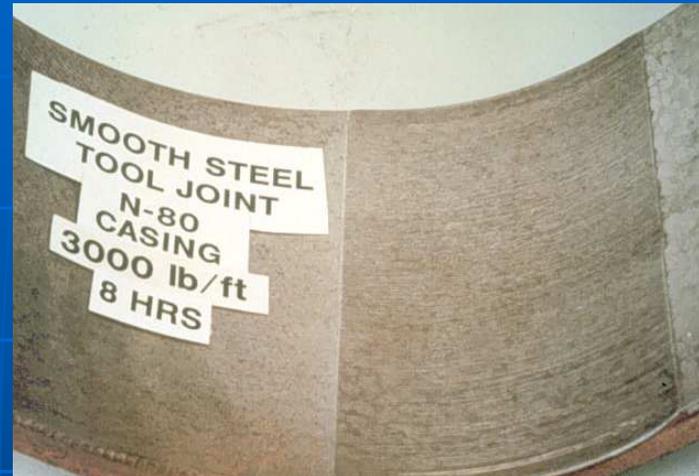
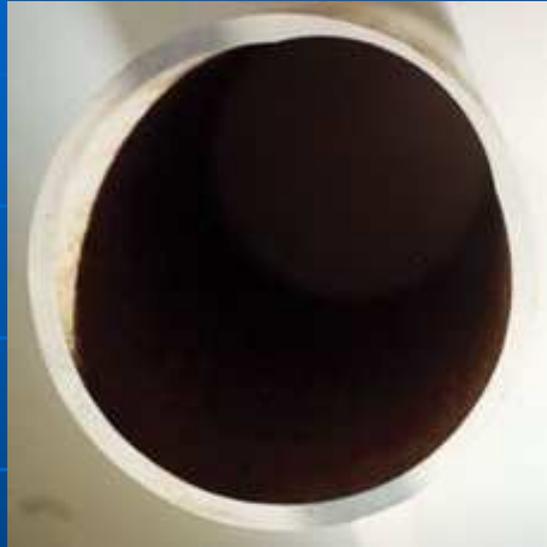
Theoretical background

- High contact pressure
- Contact area initially a line, slowly becomes a groove





Theoretical background





Affecting parameters



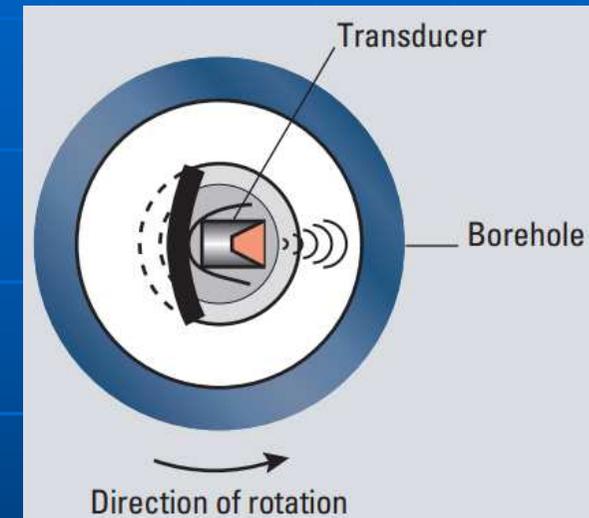
- Lateral load
- Well survey (Dogleg severity)
- Mud composition
- Tool joint hardbanding



Casing Wear logging tools



- Ultrasonic Imaging Tool
- Circumferential borehole-imaging tool





Wear mitigation



- Non-rotating drillpipe protector
- Downhole motor
- Mud additives – lubricants
- Tool-joint materials
- Internal casing coating





Remedial actions



- Complete replacement
- Partial replacement
 - Rethreading
 - Overshot
- Squeeze cementing



PetrisWinds DrillNET



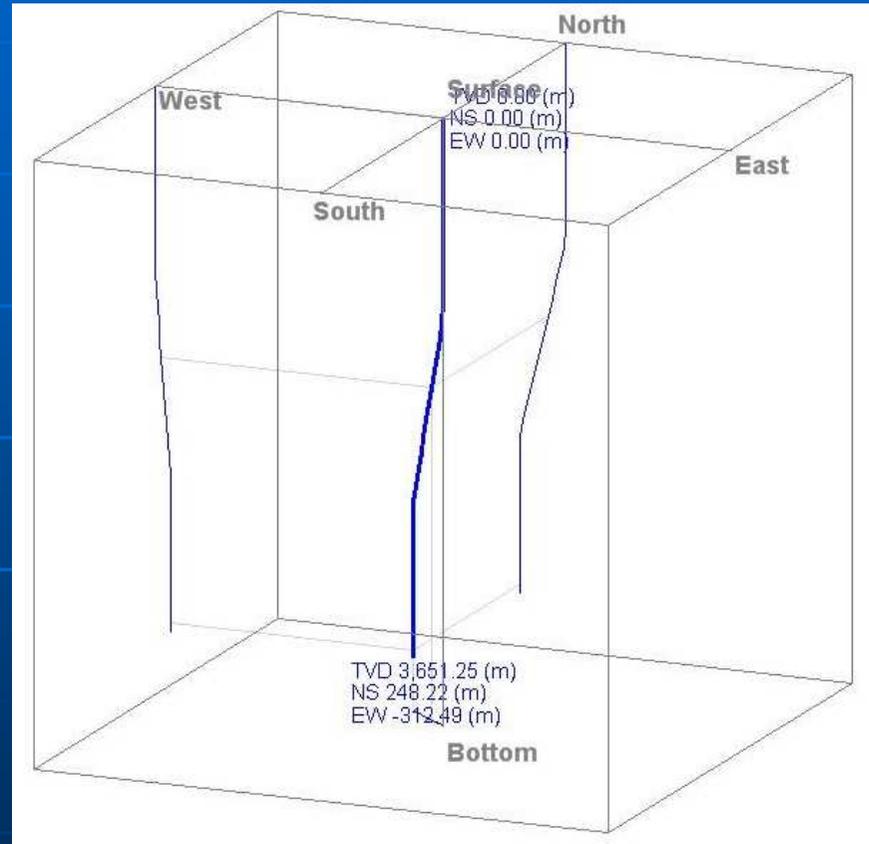
- Drilling engineering integrated analysis package
- Casing Wear module
- The model predicts the location and magnitude of casing wear in casing strings
- Calculates volumetric casing wear
- Energy based calculations



Candidate well

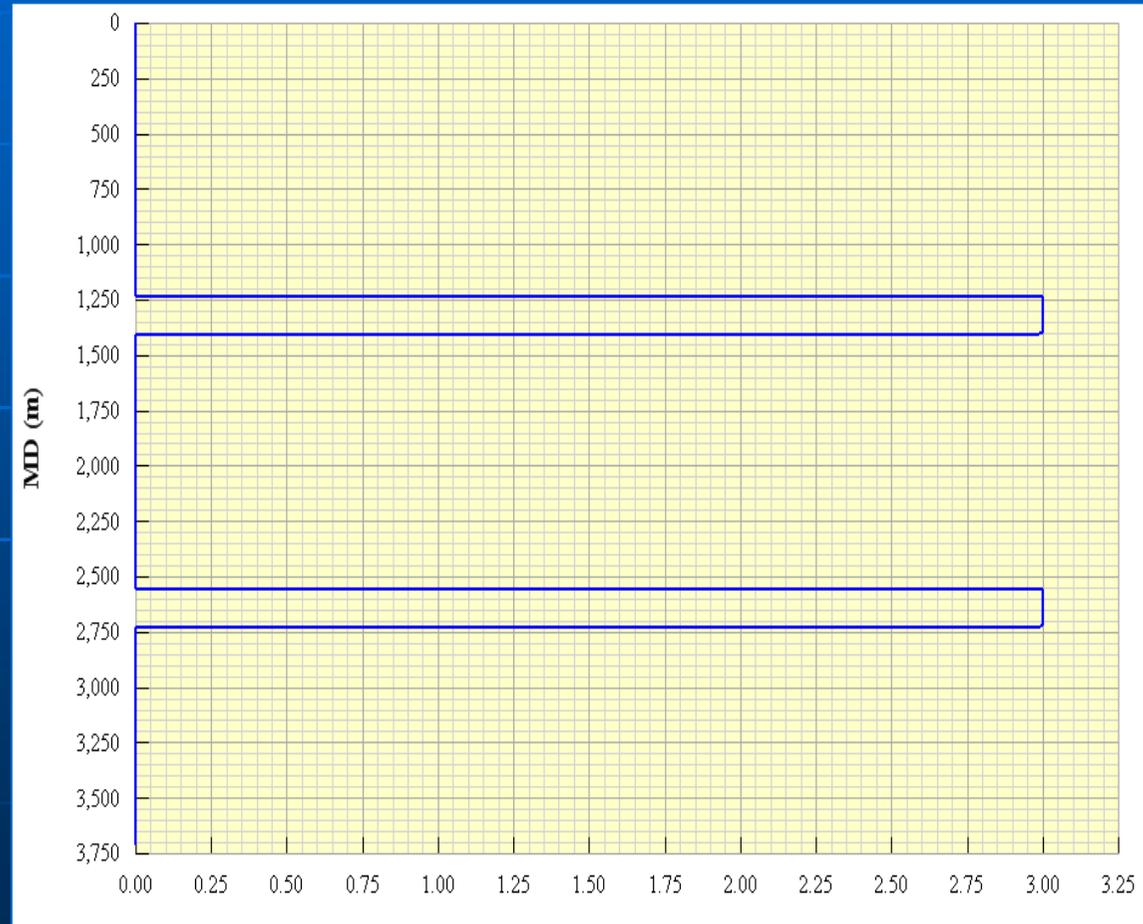
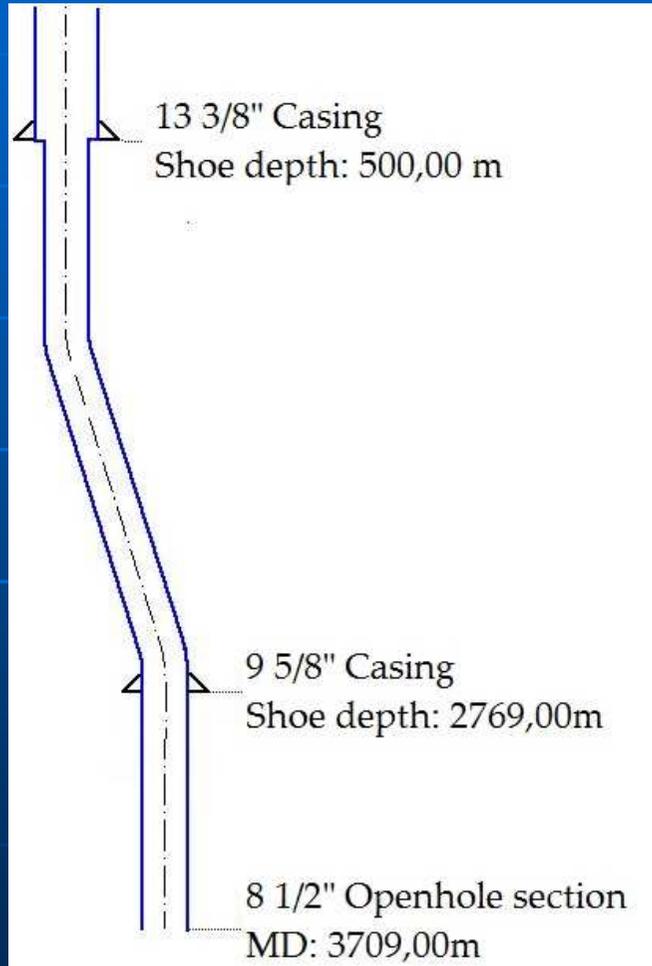


- S-shaped well
- Long radius build and drop section
- Build to $17,6^\circ$ inclination from 1240 - 1406 m
- Hold section
- Drop to vertical from 2560-2729 m





Candidate well

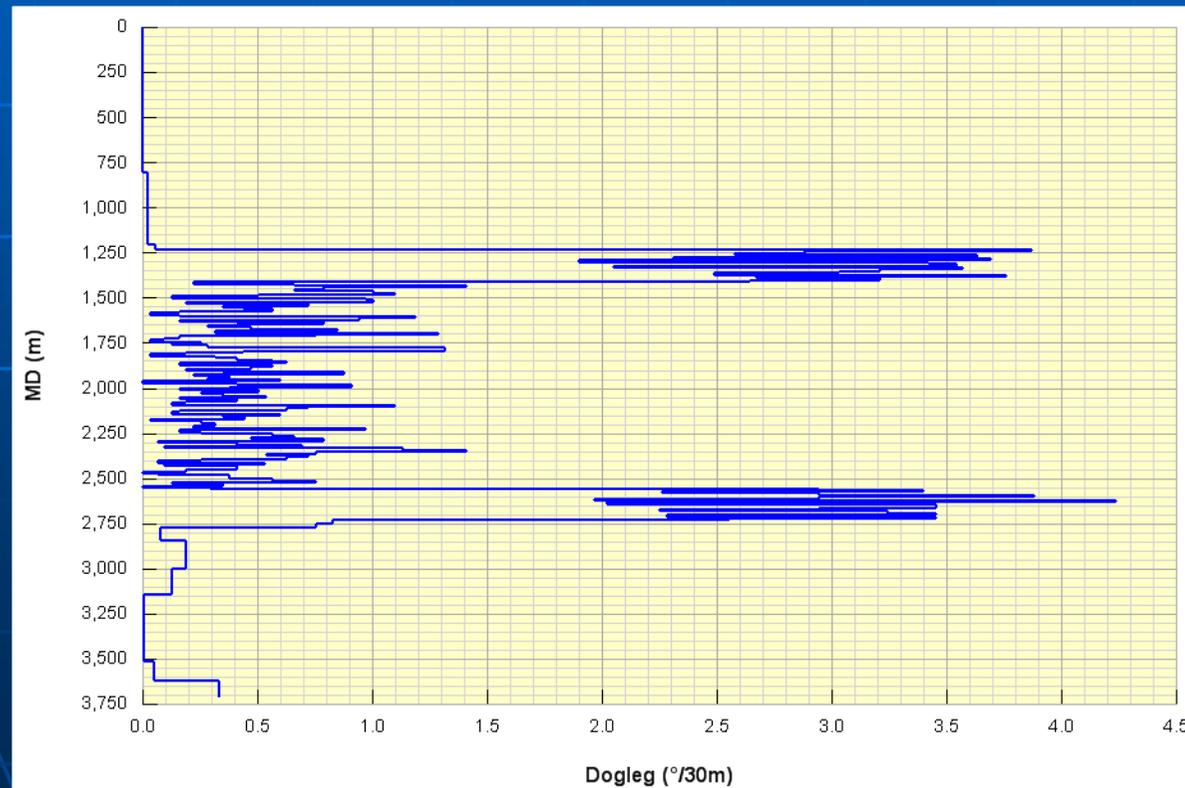




Pre-simulation work

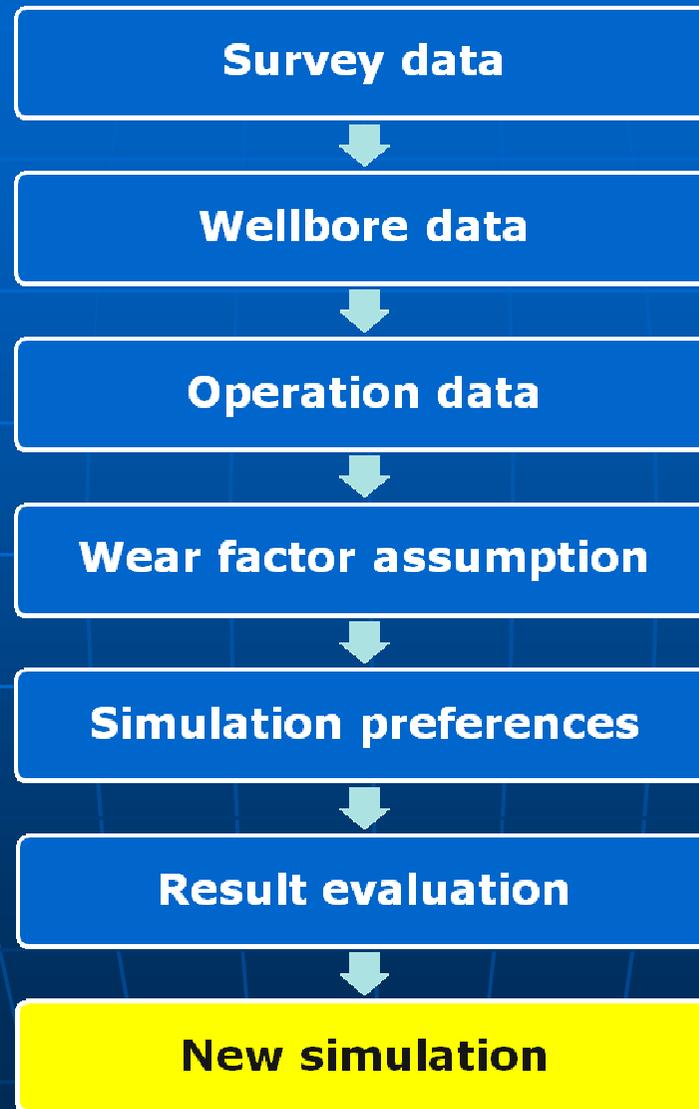


- Adding tortuosity, adjusting inclination and dogleg values





Simulation workflow





Simulation preferences

Model Options	
Wear factor input:	Single wear factor
Single wear factor input:	5.00
Wear from Drill pipe body/casing contact:	Not considered
Buckling criteria:	Dawson and Paslay
Burst and collapse:	API equation
Buckling frictional force:	Helical frictional force not considered
Bending stiffness:	Considered
Operation General Data	
Tool joint OD	6.500 (in)
Tool joint contact length	20.079 (in)
Drill pipe joint length	9.600 (m)
Drill pipe type/grade	NC50 (XH)

Drilling parameters			
Mud weight		1,1 g/cm ³	
Rotating RPM	Drilling	80 RPM	Average of rotating and sliding
	Reaming	80 RPM	After every stand
	Wiper trip	1 RPM	Every 300 m, 50 m overlap
Rate of penetration		4,5 m/h	
Weight on bit	Vertical section	4 t	
	Directional section	8 t	



Wear factor



- Represents the energy required to remove a unit volume of casing material for a given set of conditions, function of:
 - Casing and tool joint materials
 - Drilling fluid composition

Tool Joint Material

Hardmetal Steel Rubber Protector (Smooth) Rubber Protector (Fluted)

Drilling Fluids

Water Based Mud
 Oil Based Mud
 Water
 Brine
 Air

Additives

None
 Barite
 Limestone
 Iron Oxide
 HEC Polymer
 XC Polymer

Wear factor range: (E-10/psi)

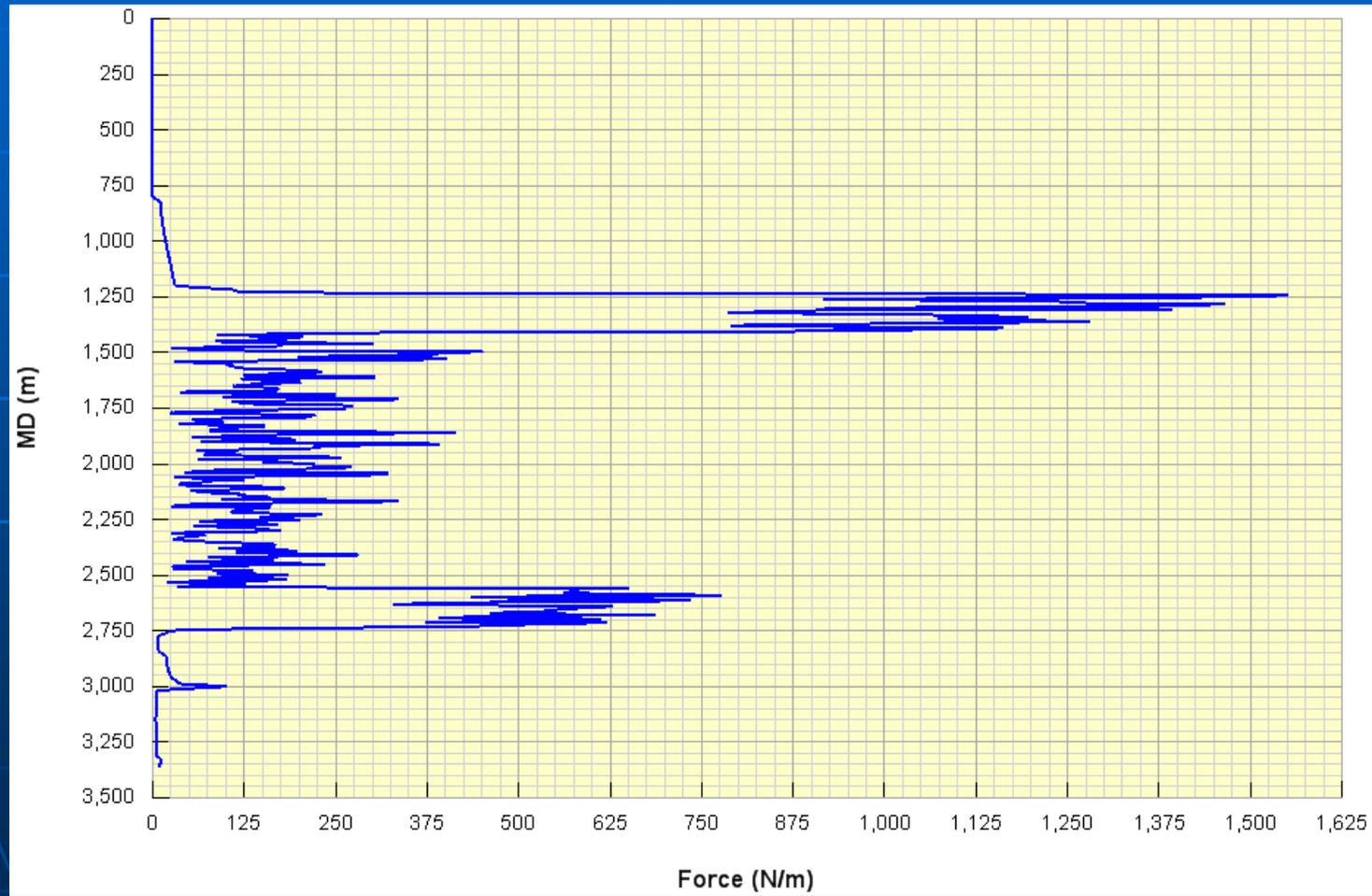
Suggested value: (E-10/psi)



Simulation results



Normal force

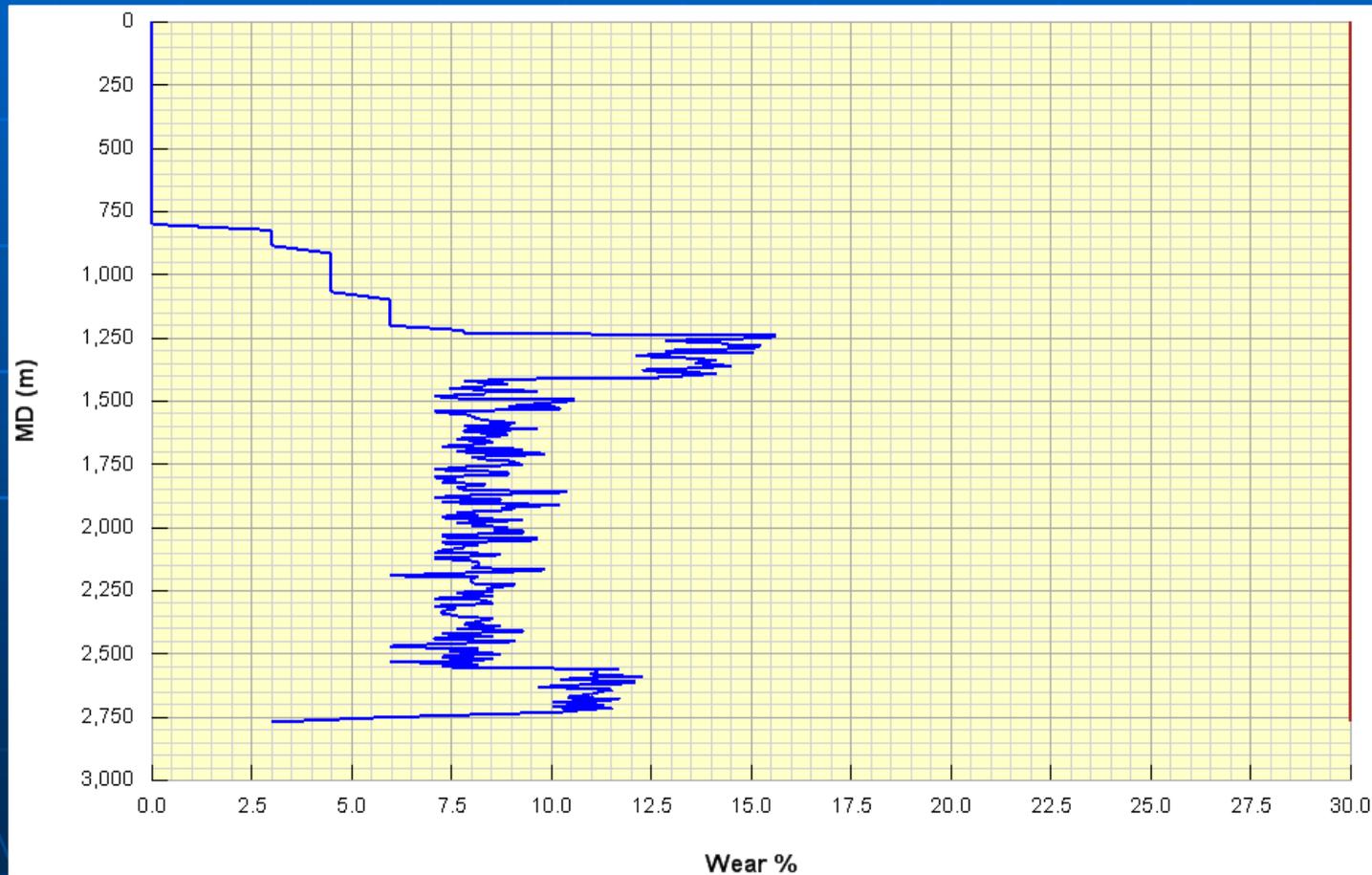




Simulation results



Wear percentage

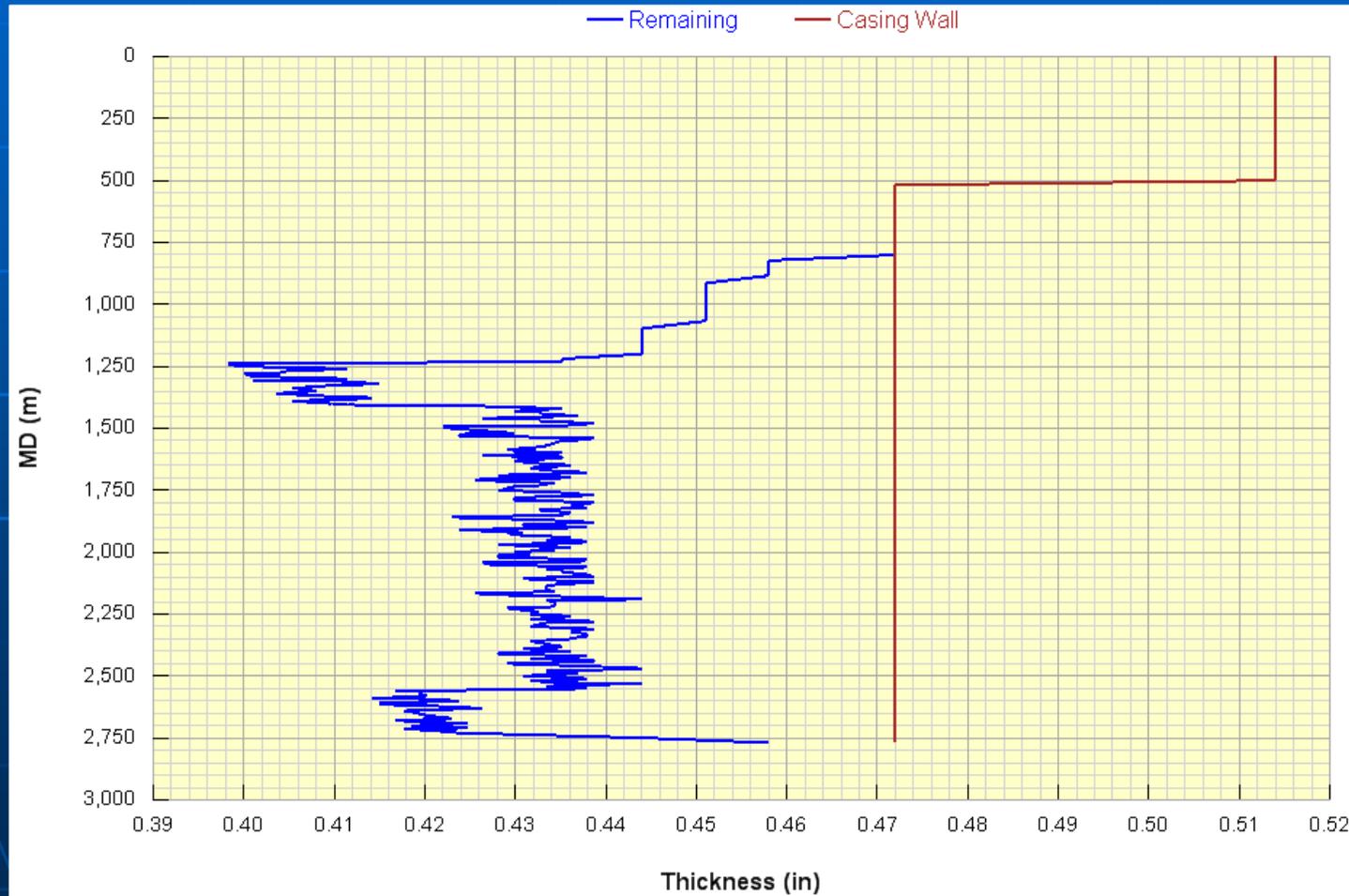




Simulation results



Reduction of casing wall thickness

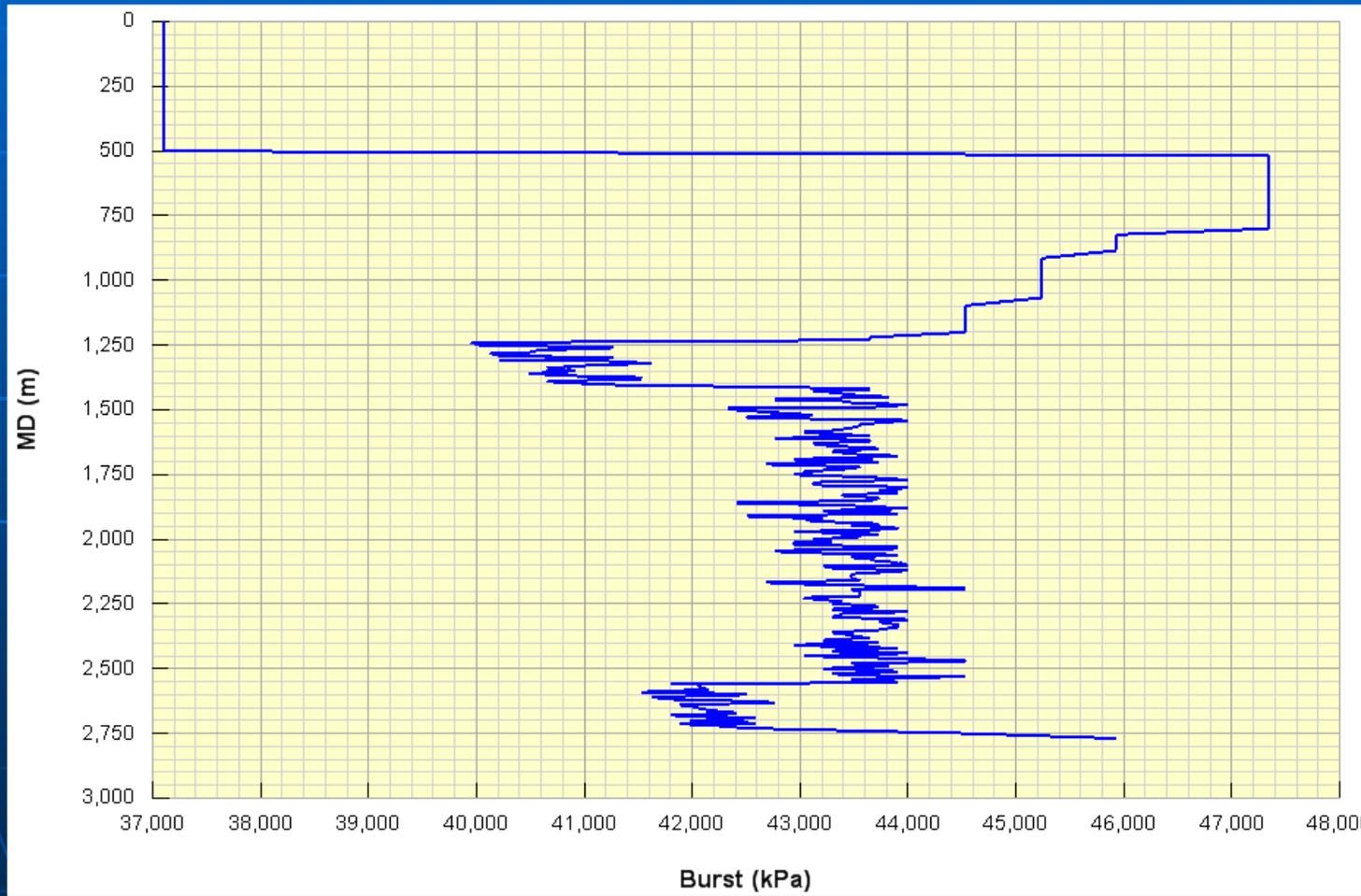




Simulation results



Burst pressure

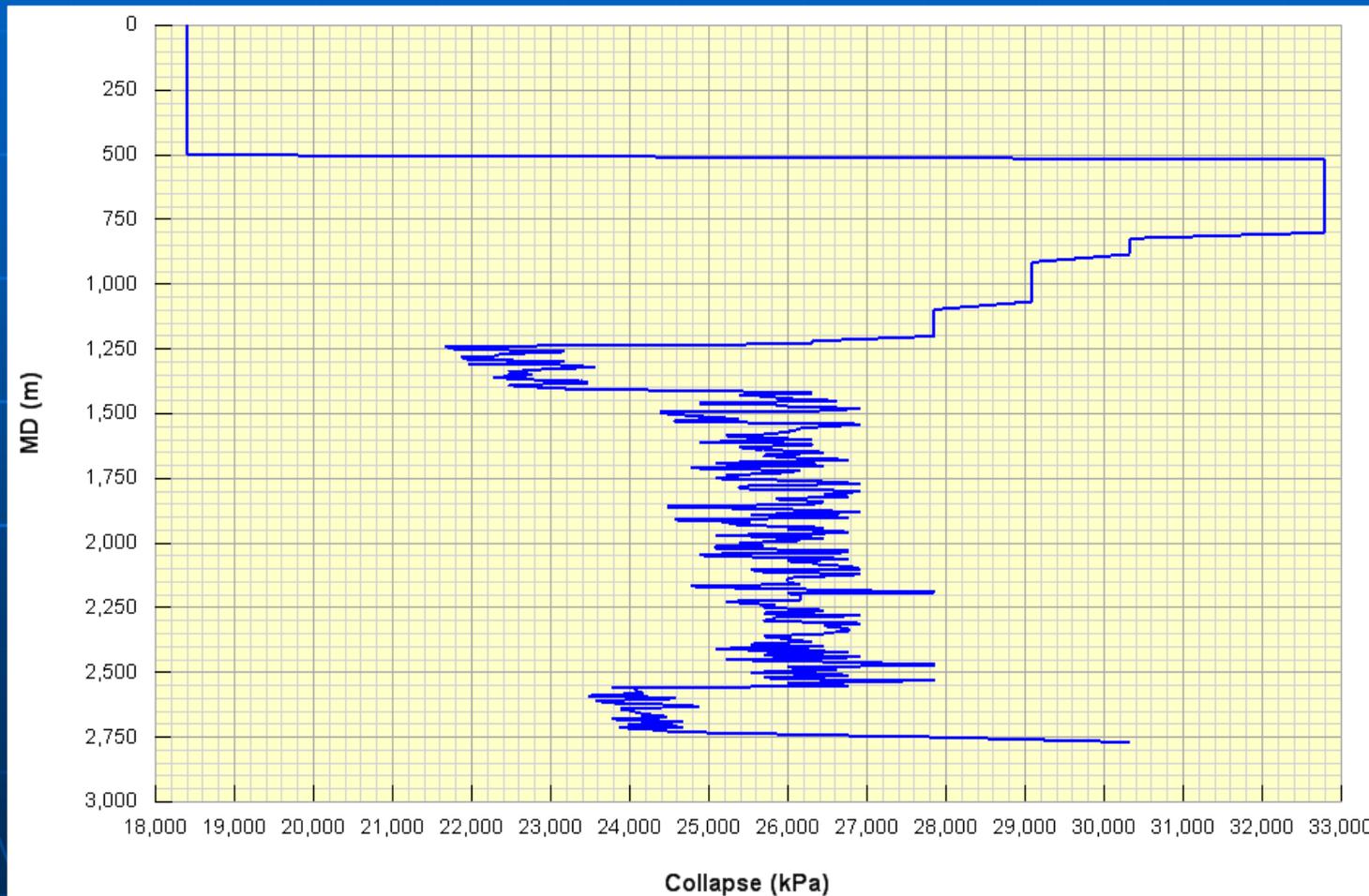




Simulation results

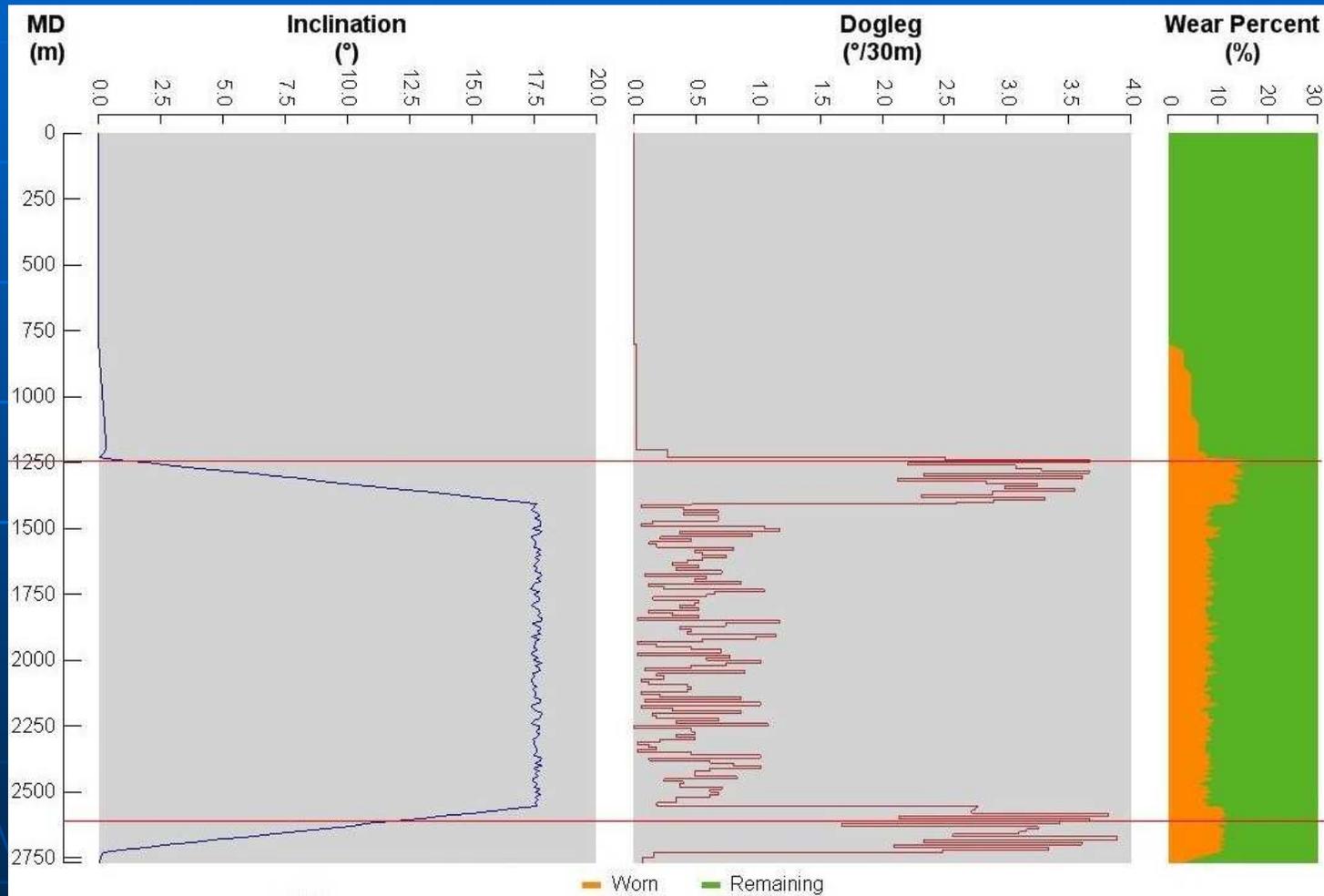


Collapse pressure





Simulation results





Conclusions



- Highest amount of wear at the highest dogleg values, where the inclination/azimuth starts to change
- Considerable reduction in casing strength even with small doglegs
- Simulations can predict the amount of casing wear during the well design process
- Casing wear can be tracked during the drilling process
- State of casing can forecast future remedial operations necessary to maintain well integrity



Thank You for your attention!

Questions?